



High Precision Continuous Flow $\delta^2\text{H}$ and $\delta^{18}\text{O}$ Analysis of Water Samples



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Background

On-line determination of $\delta^2\text{H}$ as well as $\delta^{18}\text{O}$ values from organic sample material using temperatures above 1300°C , a He carrier gas and a pool of carbon in the reaction zone has found growing interest. H- and O-containing organic material and some inorganic oxides react to H_2 and CO which are separated on a gas chromatograph and introduced into an isotope ratio mass spectrometer (IRMS).

The technique has proven successful mainly because other classical (dual inlet) means of determining $\delta^2\text{H}$ or $\delta^{18}\text{O}$ material are more tedious or more erroneous. Classical reduction techniques with U, Zn or Cr to measure $^2\text{H}/^1\text{H}$ in water with dual inlet techniques produce robust and reliable results, but require a special laboratory for measurements. On the other hand, precision of the ConFlo technique in particular for $\delta^{18}\text{O}$ values has remained an issue, mainly because of memory effects. Measurements could be made at the 0.2–0.3 ‰ level at best, which is not acceptable for water samples.

Objectives

The main objectives of the current experiments were:

- to develop a routine laboratory method for stable isotope ratio analysis of water samples
- to improve the measurement precision by reducing the sample-to-sample memory

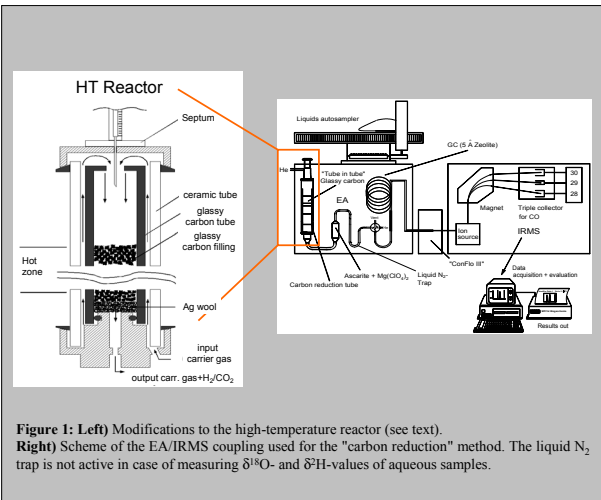


Figure 1: (Left) Modifications to the high-temperature reactor (see text). (Right) Scheme of the EA/IRMS coupling used for the "carbon reduction" method. The liquid N_2 trap is not active in case of measuring $\delta^{18}\text{O}$ - and $\delta^2\text{H}$ -values of aqueous samples.

Experimental Setup

We have modified the original setup of a high-temperature reactor (TC/EA) coupled on-line via a ConFlo III interface to a Delta^{XL} IRMS (all units from Finnigan MAT). Water is injected automatically with an A200S autosampler equipped with a gas-tight syringe. Injection of 1.0 μL water is made with two washing cycles and five pullups. The needle is left in the externally heated septum for 16 s. In order to deposit waste water the needle tip is brought into contact with filter paper inside the waste bottle.

Changes to the reactor design

Major modifications to the original system (Fig. 1):

- changes to the design of the inner glassy carbon tube
- redirection of the carrier gas flow

The original open-ended glassy carbon tube was replaced with a longer one that is closed at the top end and extends over the whole length of the outer Al_2O_3 tube. A centered 2 mm hole was drilled into the closed side.

Instead of feeding the carrier gas into the tube at the septum head, we have attached the carrier line to the new bottom connector. By sealing the glassy carbon internally using a silicone O-ring (see lower part of Fig. 1) we force the carrier gas to pass first through the outer ring space between the Al_2O_3 tube and the glassy carbon tube. At the top, helium enters through the small hole in the glassy carbon reactor cover. Due to the high linear velocity of the carrier gas through this hole, water flash evaporating from the syringe cannot escape to the top. Thus, the glassy carbon is the only wetted surface the sample water can come into contact with. This design improves the sample-to-sample memory considerably (mostly < 2). After modifying the glassy carbon tube setup, also the yield has stabilized with a variability of less than 5%.

Results

- By modifying the experimental setup, precision for $\delta^{18}\text{O}$ consistently improved to the 0.1 ‰ level.
- Memory effects within the high temperature reactor were reduced by avoiding over-spilling of evaporating water.
- Residual memory effects are corrected during post analysis evaluation (Tab. 1, Fig. 2). Memory correction considers up to eight measurements preceding the actual sample; the effect is most pronounced after a jump in isotopic composition. After manual selection of representative lab reference water injections, a usually small drift correction (=long-term memory) is applied. By comparing the reference value for our wwv-1 standard with the drift-corrected value, the offset can be determined and subsequently corrected. Finally, values are scaled to the known difference between VSMOW and SLAP.

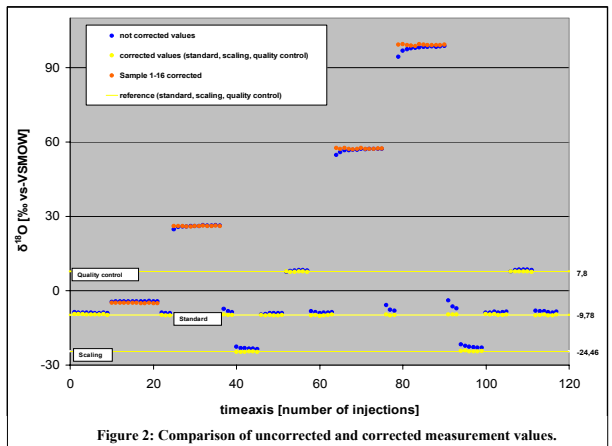


Figure 2: Comparison of uncorrected and corrected measurement values.

Sample name	Raw data $\delta^{18}\text{O}$	Linearity CO	Linearity correction	Memory correction	Forecast	Drift correction	Offset correction	Overall corr. + values incl. scaling & offset
Standard 1	7.8	7.8	7.8	7.8	7.8	7.8	7.8	7.8
Standard 2	-9.78	-9.78	-9.78	-9.78	-9.78	-9.78	-9.78	-9.78
Standard 3	-24.46	-24.46	-24.46	-24.46	-24.46	-24.46	-24.46	-24.46
Sample 1	90	90	90	90	90	90	90	90
Sample 2	60	60	60	60	60	60	60	60
Sample 3	30	30	30	30	30	30	30	30
Sample 4	0	0	0	0	0	0	0	0
Sample 5	-30	-30	-30	-30	-30	-30	-30	-30
Sample 6	-90	-90	-90	-90	-90	-90	-90	-90
Sample 7	90	90	90	90	90	90	90	90
Sample 8	60	60	60	60	60	60	60	60
Sample 9	30	30	30	30	30	30	30	30
Sample 10	0	0	0	0	0	0	0	0
Sample 11	-30	-30	-30	-30	-30	-30	-30	-30
Sample 12	-60	-60	-60	-60	-60	-60	-60	-60
Sample 13	-90	-90	-90	-90	-90	-90	-90	-90
Sample 14	90	90	90	90	90	90	90	90
Sample 15	60	60	60	60	60	60	60	60
Sample 16	30	30	30	30	30	30	30	30
Sample 17	0	0	0	0	0	0	0	0
Sample 18	-30	-30	-30	-30	-30	-30	-30	-30
Sample 19	-60	-60	-60	-60	-60	-60	-60	-60
Sample 20	-90	-90	-90	-90	-90	-90	-90	-90
Sample 21	90	90	90	90	90	90	90	90
Sample 22	60	60	60	60	60	60	60	60
Sample 23	30	30	30	30	30	30	30	30
Sample 24	0	0	0	0	0	0	0	0
Sample 25	-30	-30	-30	-30	-30	-30	-30	-30
Sample 26	-60	-60	-60	-60	-60	-60	-60	-60
Sample 27	-90	-90	-90	-90	-90	-90	-90	-90
Sample 28	90	90	90	90	90	90	90	90
Sample 29	60	60	60	60	60	60	60	60
Sample 30	30	30	30	30	30	30	30	30
Sample 31	0	0	0	0	0	0	0	0
Sample 32	-30	-30	-30	-30	-30	-30	-30	-30
Sample 33	-60	-60	-60	-60	-60	-60	-60	-60
Sample 34	-90	-90	-90	-90	-90	-90	-90	-90
Sample 35	90	90	90	90	90	90	90	90
Sample 36	60	60	60	60	60	60	60	60
Sample 37	30	30	30	30	30	30	30	30
Sample 38	0	0	0	0	0	0	0	0
Sample 39	-30	-30	-30	-30	-30	-30	-30	-30
Sample 40	-60	-60	-60	-60	-60	-60	-60	-60
Sample 41	-90	-90	-90	-90	-90	-90	-90	-90
Sample 42	90	90	90	90	90	90	90	90
Sample 43	60	60	60	60	60	60	60	60
Sample 44	30	30	30	30	30	30	30	30
Sample 45	0	0	0	0	0	0	0	0
Sample 46	-30	-30	-30	-30	-30	-30	-30	-30
Sample 47	-60	-60	-60	-60	-60	-60	-60	-60
Sample 48	-90	-90	-90	-90	-90	-90	-90	-90
Sample 49	90	90	90	90	90	90	90	90
Sample 50	60	60	60	60	60	60	60	60
Sample 51	30	30	30	30	30	30	30	30
Sample 52	0	0	0	0	0	0	0	0
Sample 53	-30	-30	-30	-30	-30	-30	-30	-30
Sample 54	-60	-60	-60	-60	-60	-60	-60	-60
Sample 55	-90	-90	-90	-90	-90	-90	-90	-90
Sample 56	90	90	90	90	90	90	90	90
Sample 57	60	60	60	60	60	60	60	60
Sample 58	30	30	30	30	30	30	30	30
Sample 59	0	0	0	0	0	0	0	0
Sample 60	-30	-30	-30	-30	-30	-30	-30	-30
Sample 61	-60	-60	-60	-60	-60	-60	-60	-60
Sample 62	-90	-90	-90	-90	-90	-90	-90	-90
Sample 63	90	90	90	90	90	90	90	90
Sample 64	60	60	60	60	60	60	60	60
Sample 65	30	30	30	30	30	30	30	30
Sample 66	0	0	0	0	0	0	0	0
Sample 67	-30	-30	-30	-30	-30	-30	-30	-30
Sample 68	-60	-60	-60	-60	-60	-60	-60	-60
Sample 69	-90	-90	-90	-90	-90	-90	-90	-90
Sample 70	90	90	90	90	90	90	90	90
Sample 71	60	60	60	60	60	60	60	60
Sample 72	30	30	30	30	30	30	30	30
Sample 73	0	0	0	0	0	0	0	0
Sample 74	-30	-30	-30	-30	-30	-30	-30	-30
Sample 75	-60	-60	-60	-60	-60	-60	-60	-60
Sample 76	-90	-90	-90	-90	-90	-90	-90	-90
Sample 77	90	90	90	90	90	90	90	90
Sample 78	60	60	60	60	60	60	60	60
Sample 79	30	30	30	30	30	30	30	30
Sample 80	0	0	0	0	0	0	0	0
Sample 81	-30	-30	-30	-30	-30	-30	-30	-30
Sample 82	-60	-60	-60	-60	-60	-60	-60	-60
Sample 83	-90	-90	-90	-90	-90	-90	-90	-90
Sample 84	90	90	90	90	90	90	90	90
Sample 85	60	60	60	60	60	60	60	60
Sample 86	30	30	30	30	30	30	30	30
Sample 87	0	0	0	0	0	0	0	0
Sample 88	-30	-30	-30	-30	-30	-30	-30	-30
Sample 89	-60	-60	-60	-60	-60	-60	-60	-60
Sample 90	-90	-90	-90	-90	-90	-90	-90	-90
Sample 91	90	90	90	90	90	90	90	90
Sample 92	60	60	60	60	60	60	60	60
Sample 93	30	30	30	30	30	30	30	30
Sample 94	0	0	0	0	0	0	0	0
Sample 95	-30	-30	-30	-30	-30	-30	-30	-30
Sample 96	-60	-60	-60	-60	-60	-60	-60	-60
Sample 97	-90	-90	-90	-90	-90	-90	-90	-90
Sample 98	90	90	90	90	90	90	90	90
Sample 99	60	60	60	60	60	60	60	60
Sample 100	30	30	30	30	30	30	30	30

Table 1: Example for post analysis evaluation of the measured $\delta^{18}\text{O}$ data (shortened extract of evaluation spreadsheet). Blue values represent uncorrected raw data, samples are highlighted in red, standard, scaling and quality control are high-lighted in yellow.